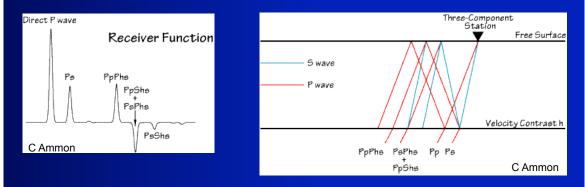


Receiver Functions – Overview

Receiver functions are time series, computed from three-component seismograms that show the response of Earth structure beneath a station. The waveform isolates P-to-S converted waves that reverberate in the structure beneath the seismometer.



Modeling the amplitude and timing of the reverberations can provide valuable constraints on the underlying geology (H, Vp/Vs). The main features of the structure can be approximated by a sequence of horizontal layers and the arrivals generated by each sharp boundary looks something sketch on the right.

http://eqseis.geosc.psu.edu/~cammon/HTML/RftnDocs/rftn01.html

Receiver Functions – an Overview

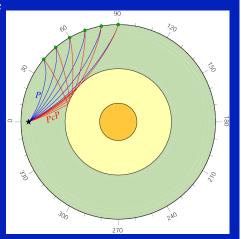
<u>Teleseismic arrival</u> – steep angle of incidence beneath the station. Vertical component is dominated by P phases; horizontal components are dominated by converted S phases.

S(t) = STF(t) * P(t) * I(t) * H(t)

S: seismogram, *STF*: earthquake source-time function, *P*: along-path effects, *I*: instrument response, *H*: receiver function.

STF, *P* and *I* are common to all 3 seismogram components. P-to-S phases *should* only be on radial component.

<u>Aim</u>: to isolate the receiver function P-to-S converted phases that carry information about the station subsurface.



Receiver Function Computation

Isolate radial receiver function by deconvolving vertical component seismogram from radial (SV) component (same procedure for tangential, SH component). In the frequency domain:

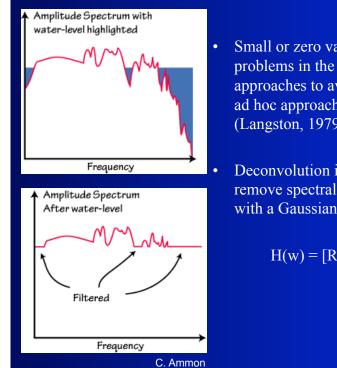
$$H(w) = R(w) / Z(w),$$

Where w is the angular frequency $2\pi f$. Z(w) and R(w) are the Fourier Transforms of the vertical and radial seismograms. This is the "source equalization approach" E.g., Ammon, (1991).

A similar equation can be written for the tangential component of motion, defining the tangential receiver function.

This is a simple concept, but in reality, reliable implementation is difficult because of the instability of deconvolution.

Water Level Deconvolution (Langston, 1979)



Small or zero values of Z(w) cause numerical problems in the calculation. There are several approaches to avoid this problem, the simplest is the ad hoc approach called water-level deconvolution. (Langston, 1979)

Deconvolution includes a 'water-level' parameter to remove spectral holes, and the result is convolved with a Gaussian filter G(w):

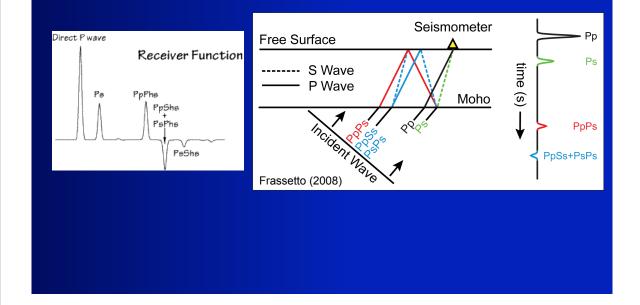
 $H(w) = [R(w) Z^{*}(w) / Z(w)Z^{*}(w)] G(w).$

Other Receiver Function Methods

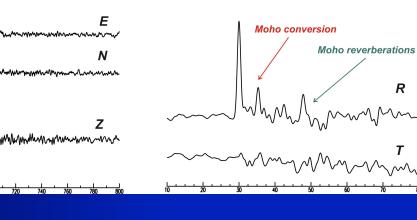
Other methods include:

- Deconvolution in the time domain by least squares (e.g., Abers et al., 1995).
- Iterative deconvolution in the time domain (e.g., Ligorria & Ammon, 1999).
- Multi-taper frequency-domain cross-correlation receiver function (MTRF), Park & Levin (2000). MTRF is more resistant to noise so better for ocean island environments, for example. This advantage is due to the use of multitapers to minimize spectral leakage and its frequency dependent down-weighting in noisy portions of the spectrum.
- Helffrich (2006) further developed the MTRF method to focus on crustal and transition zone structures – ETMTRF: Extended Time Multitaper Frequency Domain Cross-Correlation Receiver Function Estimation.

What Receiver Functions can tell us about the Earth

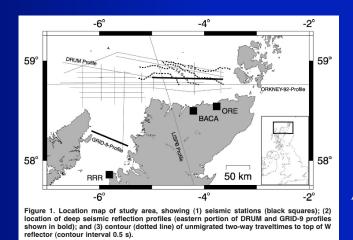


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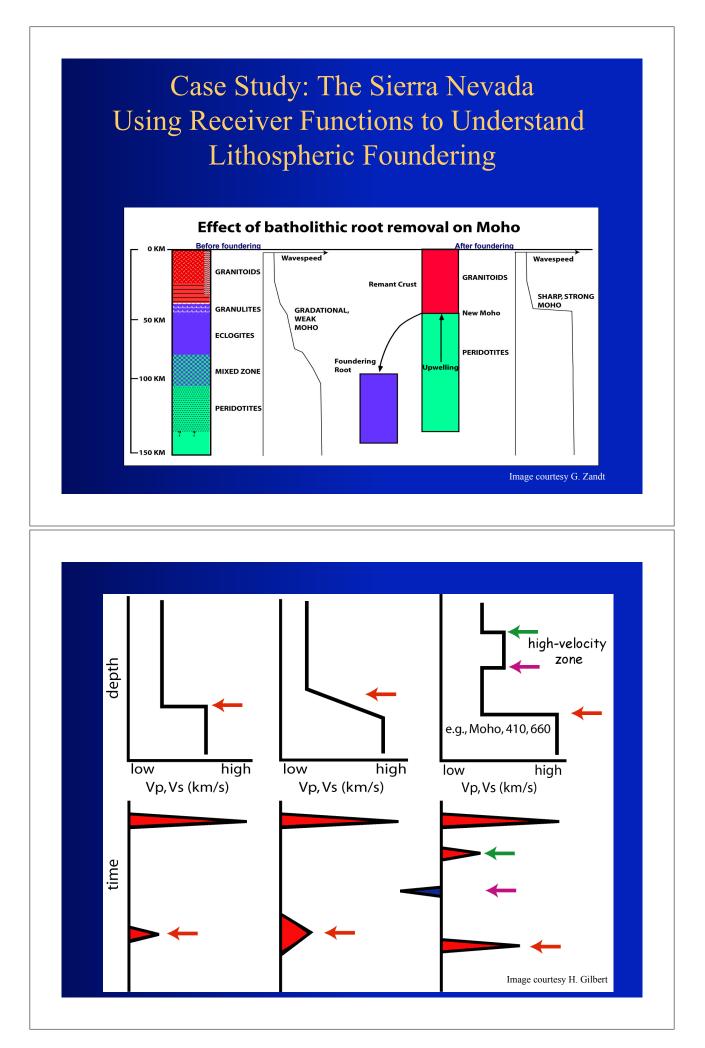
Case Study: Offshore Scottish Highlands

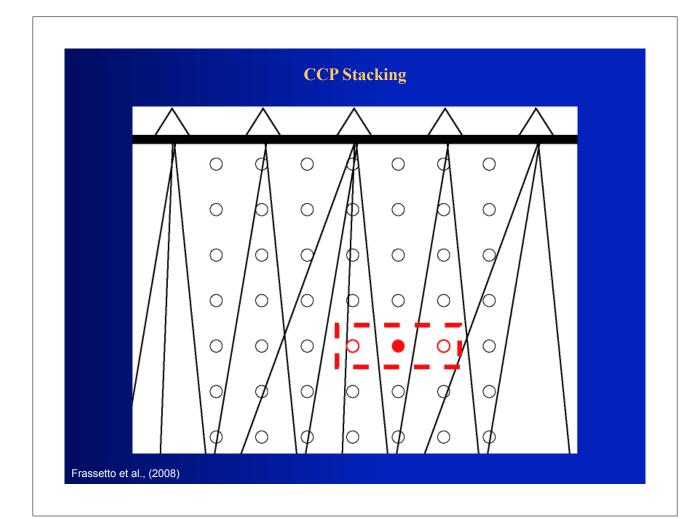
Comparisons with controlled source data



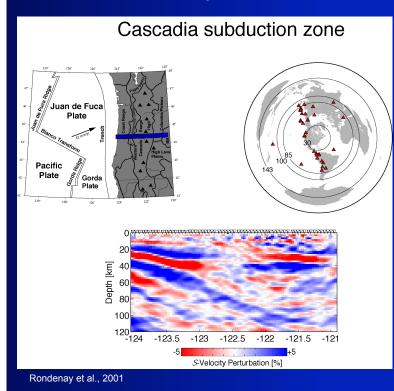
Asencio et al., (2003)

Mantle Reflectors - the W and Flannan (A) DRUM Profile—ORE Station Receiver Functions Back azimuth West East 270 315 45 90 135 BACA ORE 30 km S (S) S. 5 traveltime Moho 10 10 W-reflector VBV av -OM 15 15 0 20 20 20 km (B) GRID-9 Profile-RRR Station Receiver Functions Back azimuth NW SE 270 315 0 45 90 135 RRR (S) 40 km raveltime Moho Two-way 10 A-reflecto Flannar 15 20 km Figure 3. Correlation of radial component of receiver functions (as function of event back Asencio et al., (2003) azimuth) at (A) ORE station with major reflectors on DRUM deep seismic reflection profile and (B) RRR station with major reflectors on GRID-9 deep seismic reflection profile. Vertical scale is two-way traveltime in seconds.



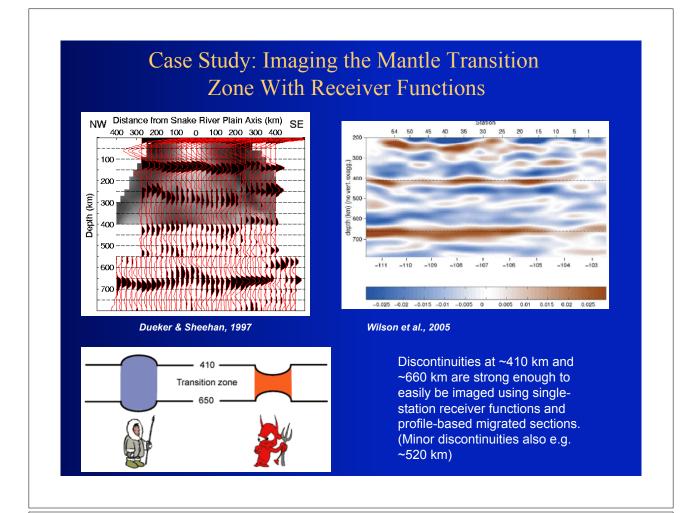


Case Study – Cascadia Subduction Zone



Calculate receiver function stacks for all stations along a dense array; carry out migration to convert time to depth \rightarrow detailed images of subsurface discontinuities

Features: continental Moho, subducting Juan de Fuca slab, mineralogical changes (basalt to eclogite; different velocity properties)

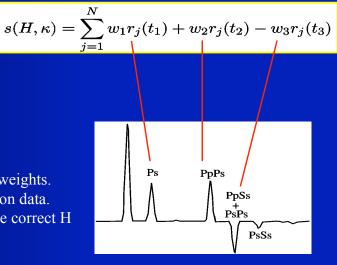


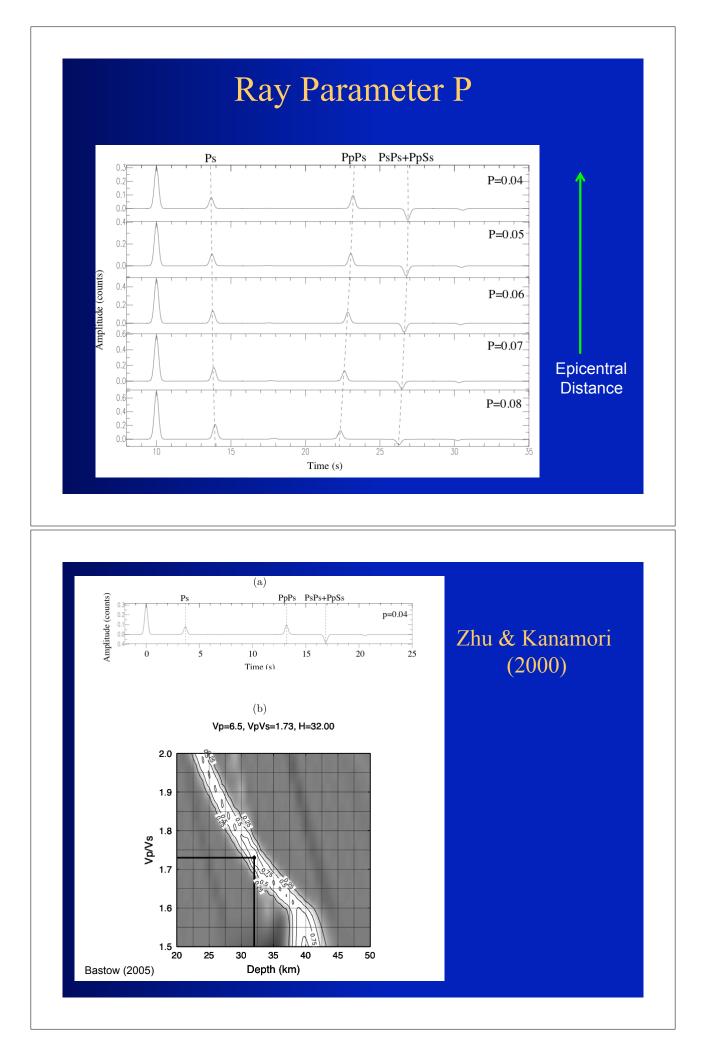
Bulk Crustal Properties

- Н-к stacking method of Zhu & Kanamori (2000).
- Crustal thickness and Vp/Vs (κ) trade-off strongly.

$$\begin{split} t_1 &= H\left[\sqrt{\frac{1}{V_S^2} - p^2} - \sqrt{\frac{1}{V_P^2} - p^2}\right] \\ t_2 &= H\left[\sqrt{\frac{1}{V_S^2} - p^2} + \sqrt{\frac{1}{V_P^2} - p^2}\right] \\ t_3 &= 2H\sqrt{\frac{1}{V_S^2} - p^2} \end{split}$$

W1 (0.6), W2 (0.3), W3 (0.1) are weights. Vp may be constrained by refraction data. $s(H,\kappa)$ should be a maximum at the correct H and Vp/Vs.





Bulk Crustal Properties H, Vp/Vs

Can relate Vp/Vs to Poisson's ratio.

Chevrot & Van der Hilst (2000)

$$\sigma = \frac{1}{2} \left[\frac{\left(\frac{V_P}{V_S}\right)^2 - 2}{\left(\left(\frac{V_P}{V_S}\right)^2 - 1\right)} \right]$$

Quartz: $\sigma = 0.09$

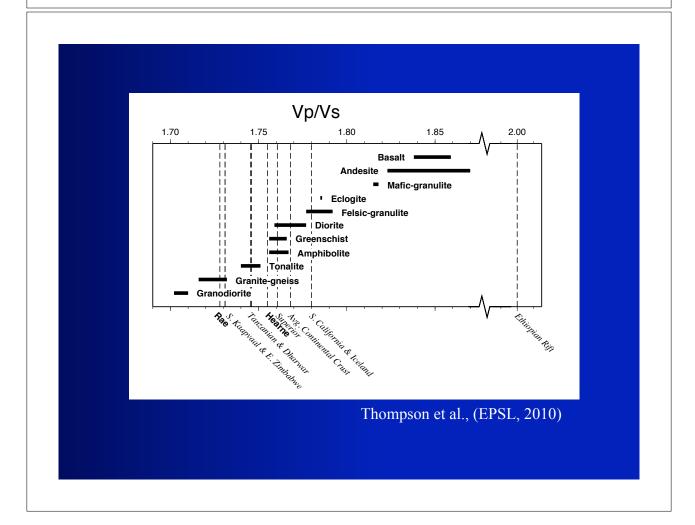
Plagioclaise Feldspar: $\sigma = 0.3$

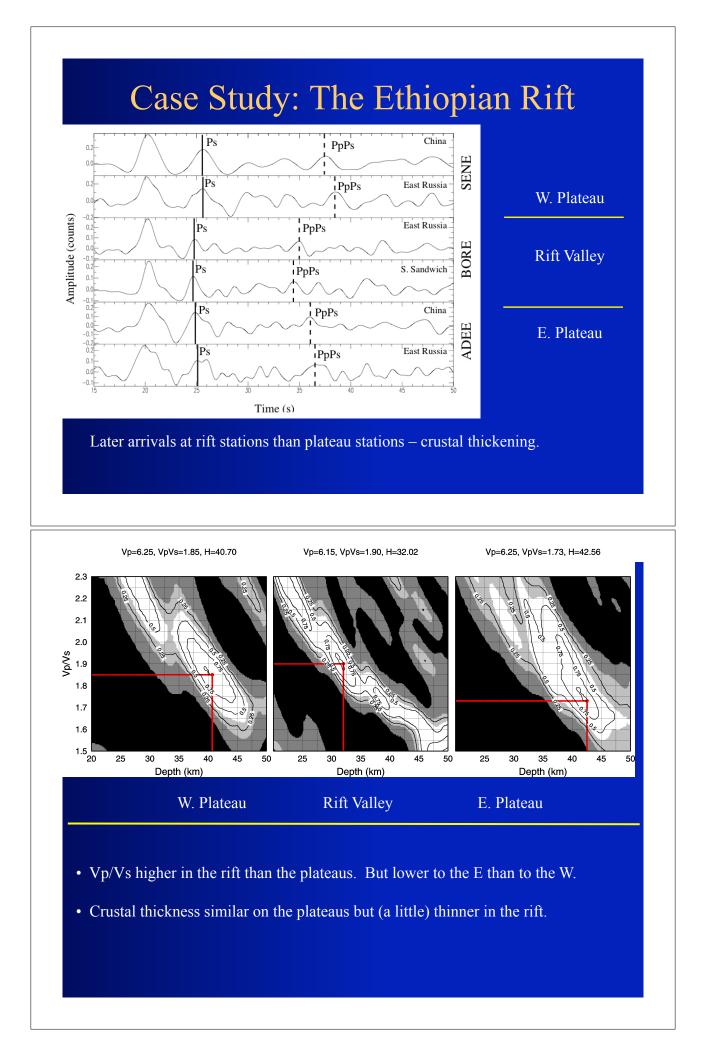
The abundance of these minerals controls bulk Poisson's ratio for many rocks.

Granite: 0.24

Diorite: 0.27

Gabbro: 0.30





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